

Basic principles of steel structures

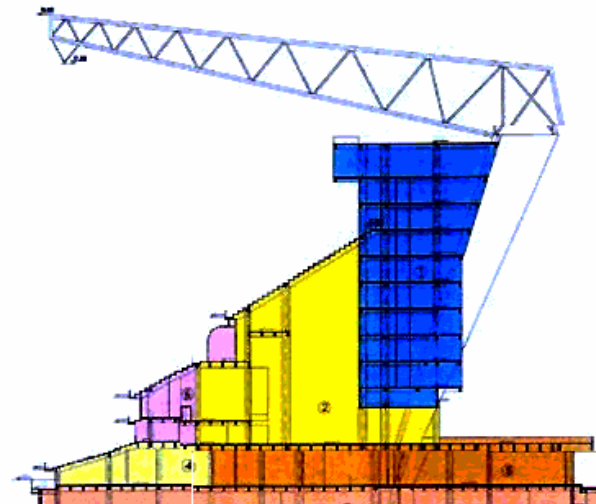
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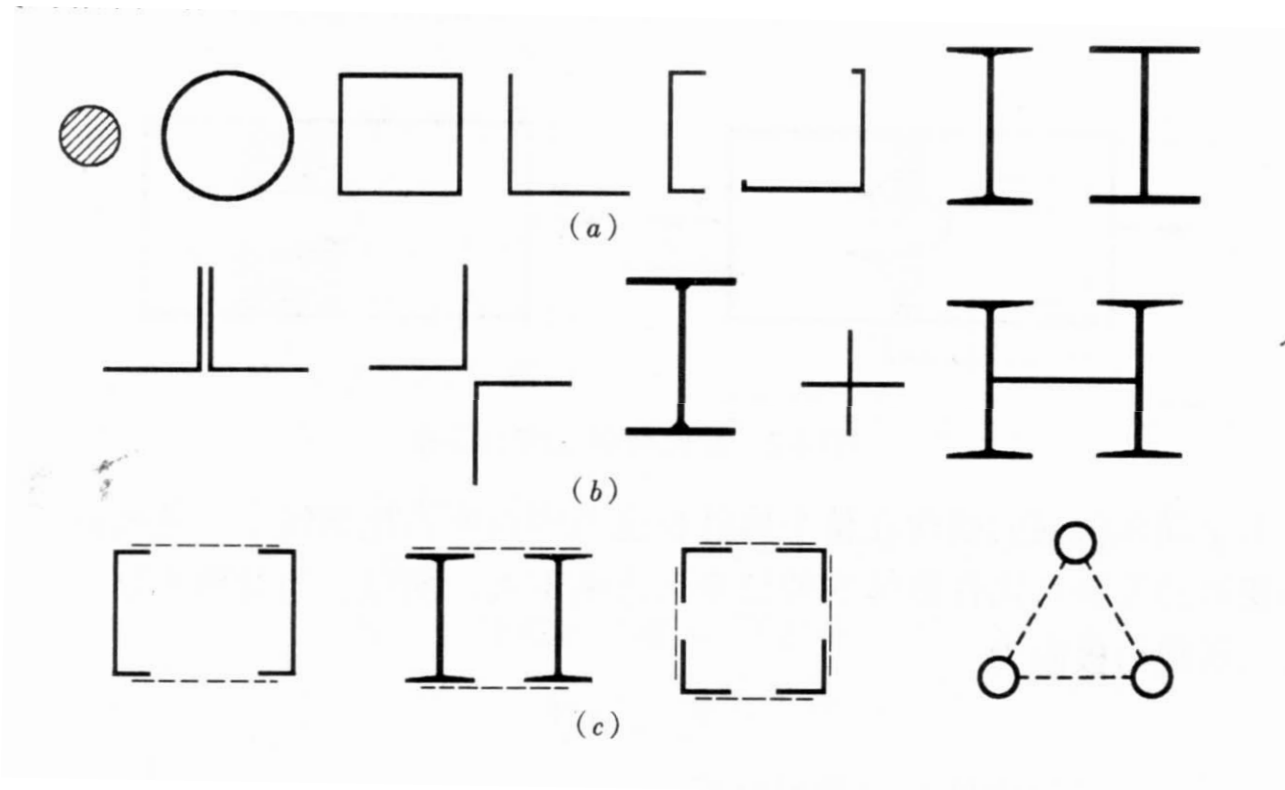
Tension members

Outlines

- ✧ (axially loaded) tension member
- ✧ member subjected to tension and bending moment
- ✧ cable



Tension members common used sections



Tension members

resistance of cross section

- ☑ Resistance of cross section for tension member

(1) for yielding in the gross section

$$N_p = Af_y$$

(2) for fracture in the net section

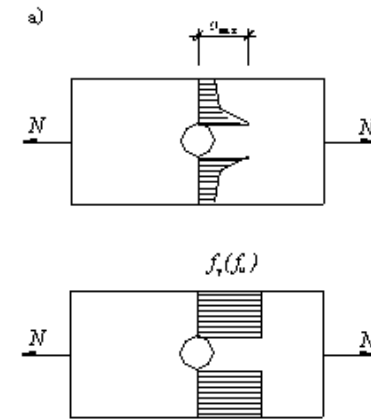
$$N_u = A_n f_u$$

Practical design equation

$$N \leq \min(N_p, N_u)$$

- ☑ Design equation in design code

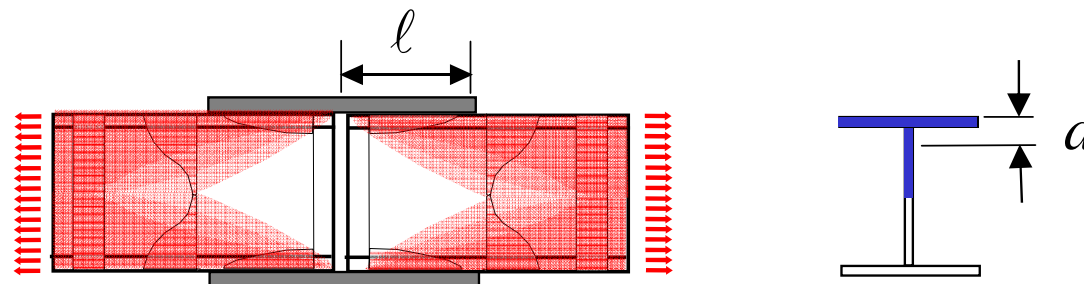
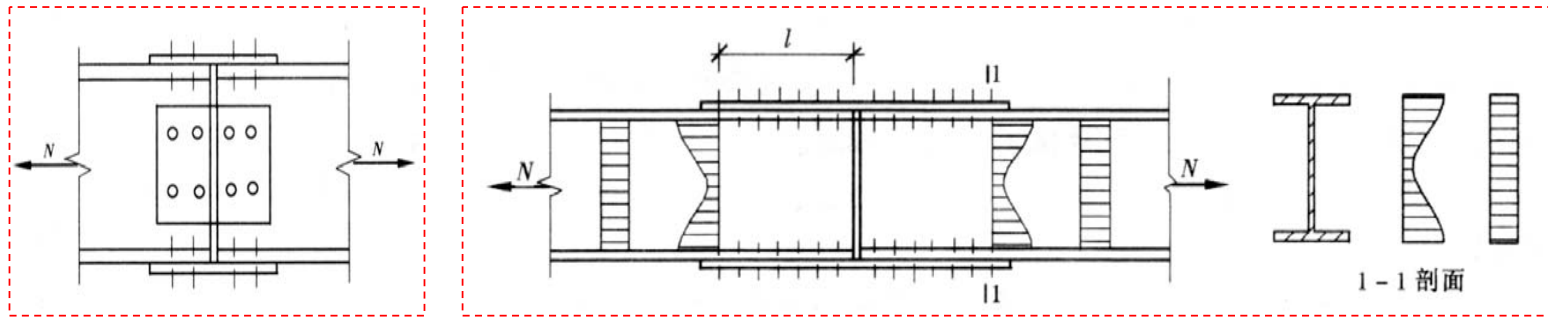
$$N \leq A_n f_d, \quad f_d = f_y / \gamma_R \quad \longrightarrow \quad \sigma = \frac{N}{A_n} \leq f_d$$



Tension members

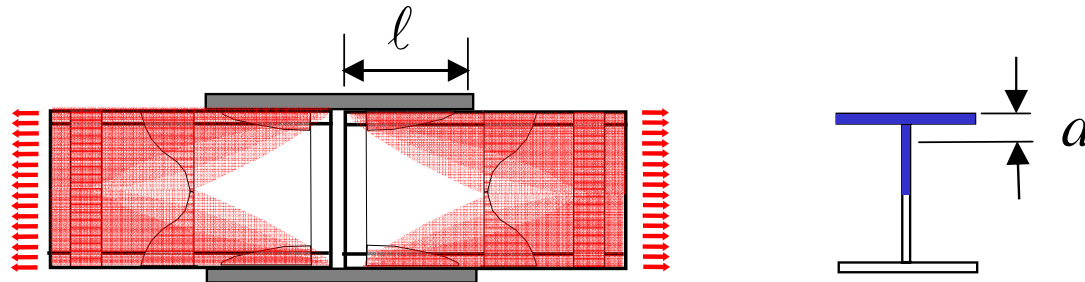
section efficiency

- ✓ Section efficiency: the ratio of the net section area enabling to transfer load to the area of net section



Tension members

section efficiency



- ✓ Factor of section efficiency

$$\eta = 1 - a / l$$

a — distance of centroid of connected area to the connection interface

l — the length of connection

- ✓ Design equation

$$\frac{N}{\eta A_n} \leq f_d$$

Tension members

rigidity of members

☑ Rigidity of member

Ability to resist the deformation of member

Elastic rigidity used in real work

☑ Rigidity of tension member

Prevent excessive deformation during fabrication, transportation, erection and usage

In fact, it's bending deflection

☑ Check the rigidity of member: control the slenderness

$$\lambda \leq [\lambda]$$

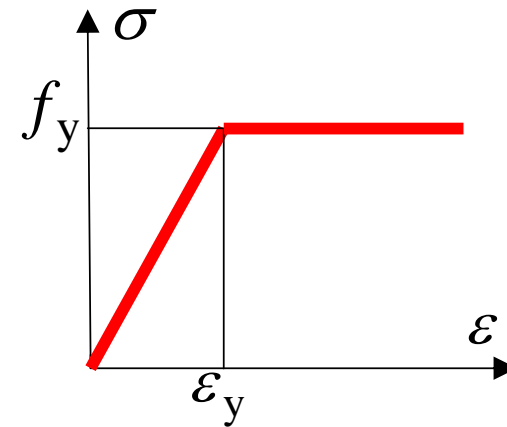
$$\lambda = \max\{\lambda_x, \lambda_y\} = \max\{\mu_x l_x / i_x, \mu_y l_y / i_y\}$$

why not control EA/L for tension member?

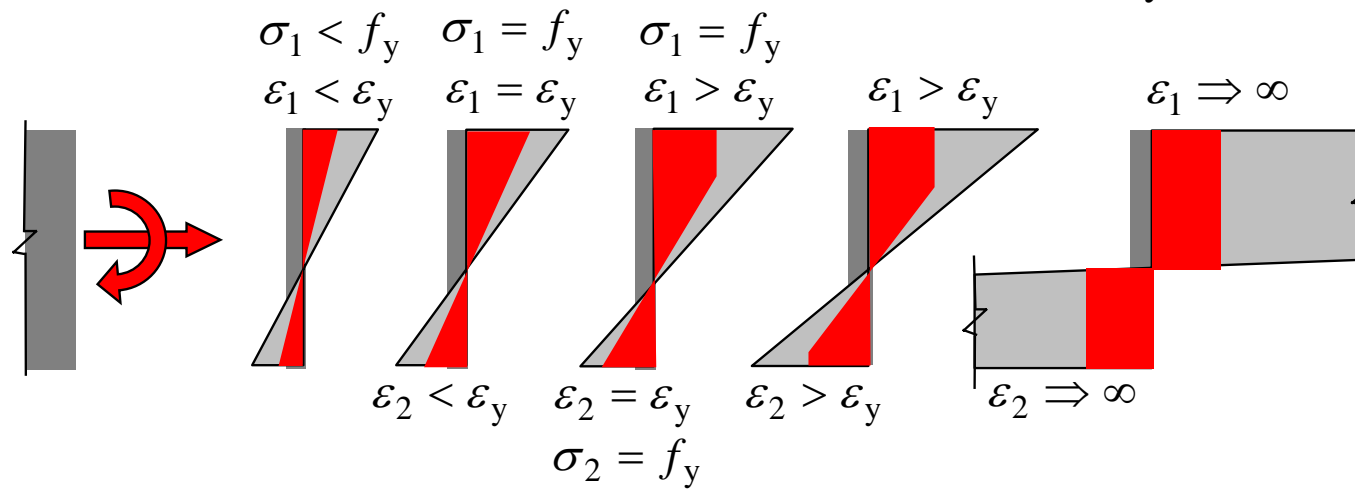
Tension members with bending diagram of strain & stress distribution

☑ assumption

- perfect elasto-plastic model
- cross section remains plane during bending



☑ distribution of normal strain and stress

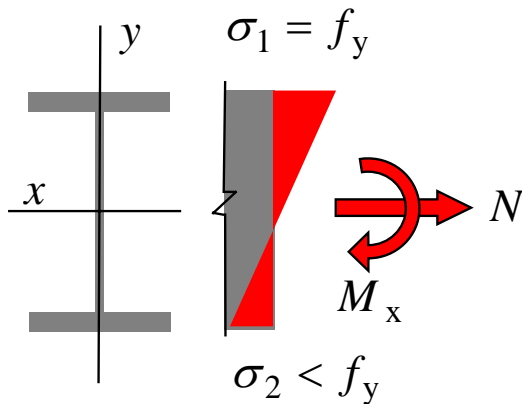


Tension members with bending criteria of yielding at extreme fibre

- ✓ Description of failure criteria

The maximum stress at the top or bottom extreme fibre reach yield point (as limit state)

- ✓ Resistance of cross-section



$$\sigma_1 = \frac{N}{A} + \frac{M_x}{W_x} \leq f_y$$

Let yield tension

$$N_p = Af_y$$

yield moment

$$M_{ex} = W_x f_y$$

then

$$\frac{N}{N_p} + \frac{M_x}{M_{ex}} \leq 1$$

- ✓ Design equation

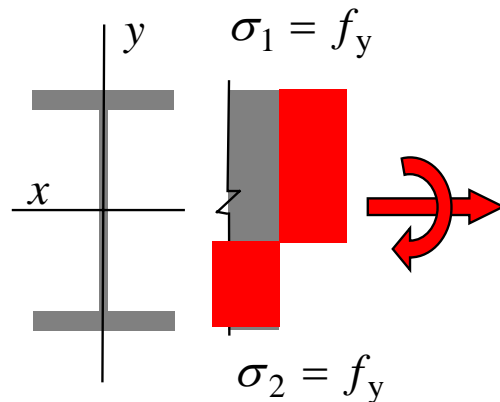
$$\frac{N}{A_n} + \frac{M_x}{W_{xn}} \leq f_d$$

Tension members with bending criteria of yielding on full section

- ✓ Description of failure criteria

The stress at each point of the section reach yield point

- ✓ Resistance of cross-section



Let yield tension $N_p = Af_y$
plastic moment $M_{px} = W_{px} f_y$
Then we get

$$A\left(\frac{N}{N_p}\right)^\alpha + B\left(\frac{M_x}{M_{px}}\right)^\beta = 1$$



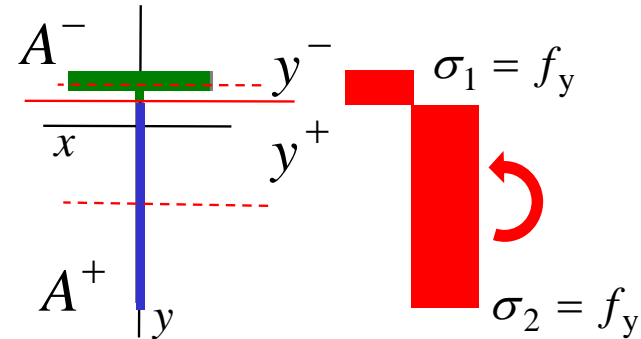
- coefficient A, B, α , β is related to section
- convex curve in N-M plane

Tension members with bending

concept of full plastic moment

☑ Assumption of stress distribution

- subjected to bending only, no tension
- stress at each point reach yield point
- yield point under tension and compression is the same



☑ Plastic neutral axis

$$N = 0 \quad \longrightarrow \quad A^+ f_y - A^- f_y = 0 \quad \longrightarrow \quad A^+ = A^-$$

The plastic neutral axis divides the cross section into two equal areas, and it may not coincide with the centroidal axis

☑ (Full) plastic moment

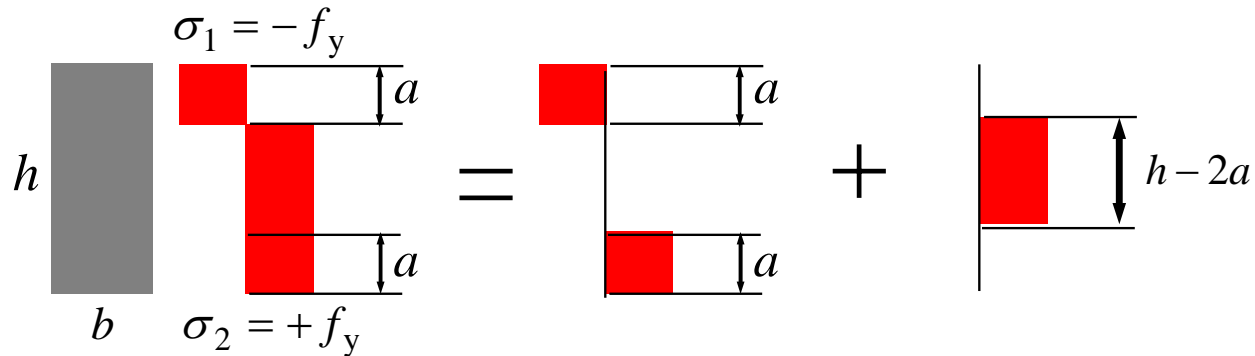
$$M_{px} = A^+ f_y y^+ + A^- f_y y^- = (A^+ y^+ + A^- y^-) f_y$$

section modulus of plastic bending:

$$W_{px} = A^+ y^+ + A^- y^-$$

$$M_{px} = W_{px} f_y$$

Tension members with bending interaction equation of tension and bending



equation of equilibrium: $N = (h - 2a)bf_y = (1 - 2a/h)N_p$ (1)

$$M_x = abf_y(h - a) = M_{px} 4[a/h - (a/h)^2] \quad (2)$$

where, $N_p = bhf_y$ $M_{px} = (1/4)bh^2 f_y$

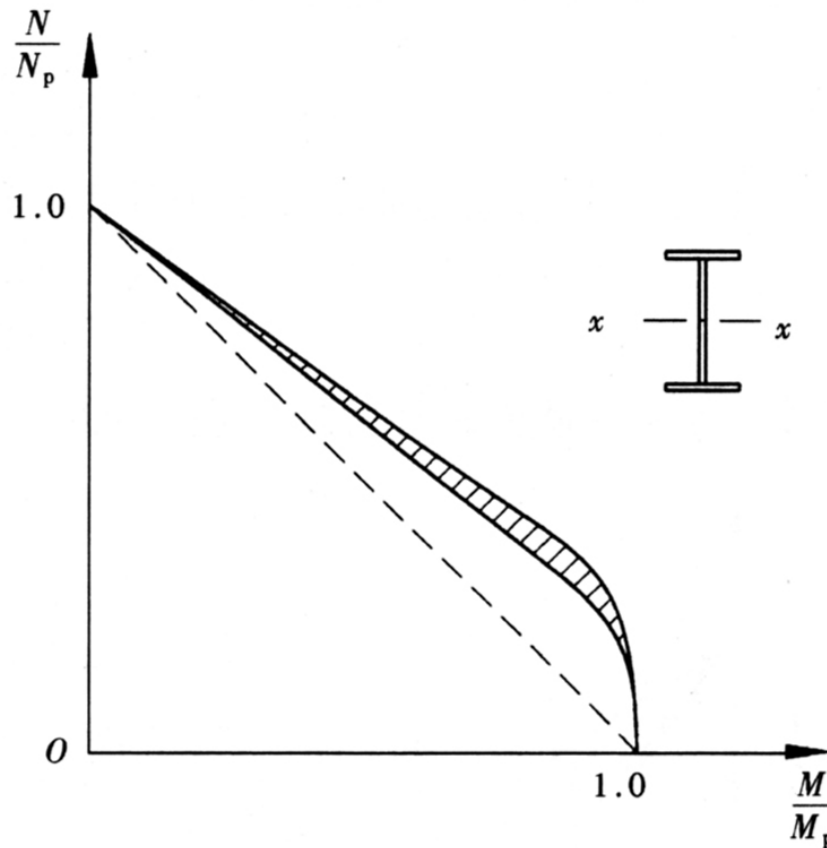
from equ. (1) $a/h = 0.5(1 - N/N_p)$

substitute to equ. (2) $M_x/M_{px} = 4 \times 0.5(1 - N/N_p)[1 - 0.5(1 - N/N_p)]$
 $= 1 - (N/N_p)^2$

finally we get: $(\frac{N}{N_p})^2 + \frac{M_x}{M_{px}} = 1$

Tension members with bending criteria of yielding on full section

- ☑ Interaction of tension and bending for I shape



$$A\left(\frac{N}{N_p}\right)^\alpha + B\left(\frac{M_x}{M_{px}}\right)^\beta = 1$$

$$\frac{N}{N_p} > 0.13, \quad \frac{N}{N_p} + \frac{M_x}{1.15M_{px}} = 1$$

$$\frac{N}{N_p} \leq 0.13, \quad \frac{M_x}{M_{px}} = 1$$



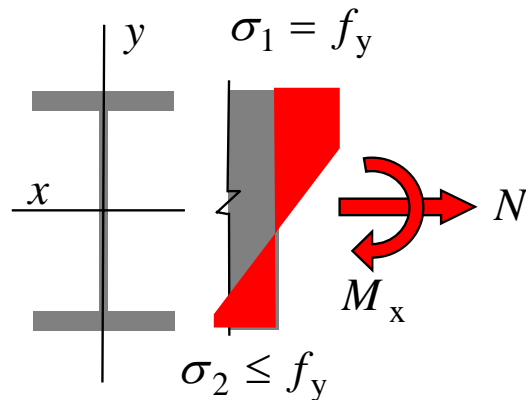
$$\frac{N}{N_p} + \frac{M_x}{M_{px}} = 1$$

Tension members with bending criteria of yielding on partial section

- ☑ Description of failure criteria

The stress at the top or/and bottom part reach yielding

- ☑ Resistance of cross-section



$$\frac{N}{A} + \frac{M_x}{\gamma_x W_x} \leq f_y$$



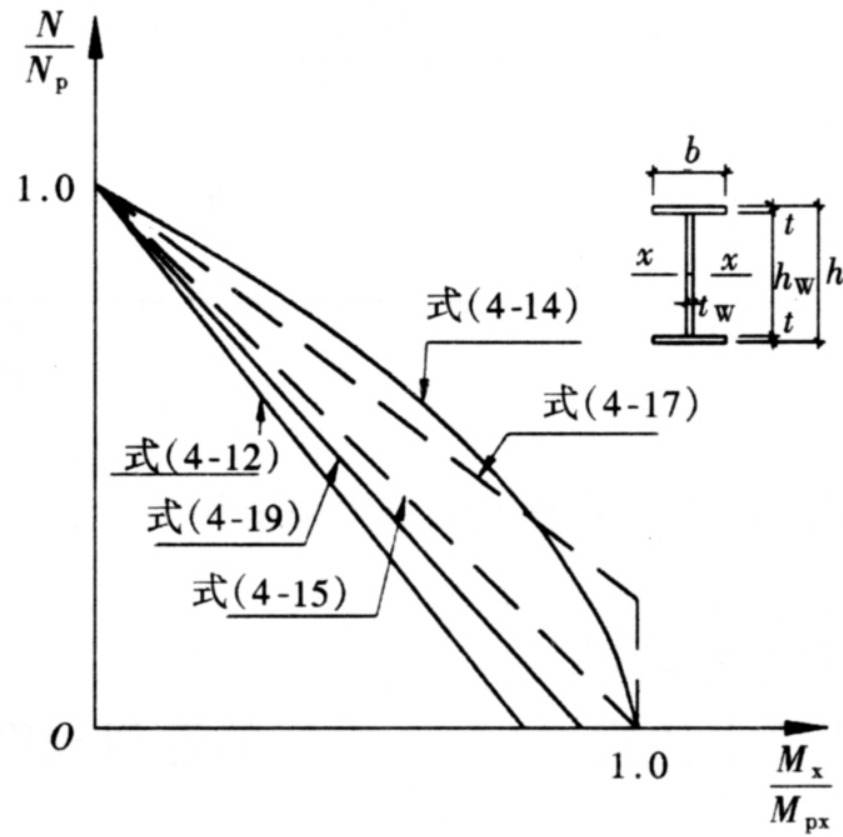
$$\frac{N}{N_p} + \frac{M_x}{\gamma_x M_{ex}} \leq 1$$

where, $\gamma_x \geq 1$

- ☑ Design equation

$$\frac{N}{A_n} + \frac{M_x}{\gamma_x W_{xn}} \leq f_d$$

Tension members with bending comparison of three criteria



Tension members with bending

rigidity and buckling

☑ Rigidity of members

- same as the tension member if tension is large
- check the deflection if bending is large

☑ Stability of members

If bending is large enough to make part area in compression

- possibility of overall buckling
- possibility of local buckling

Cable

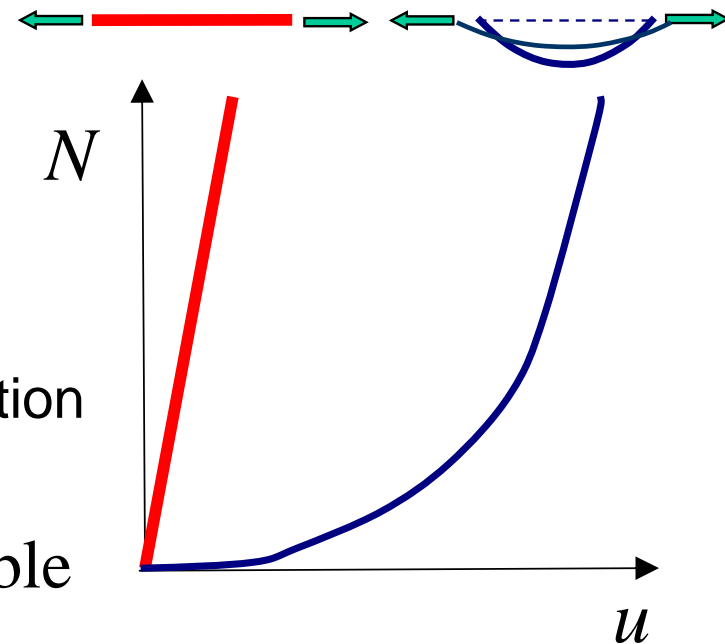
axially loaded rigid bar and cable

- ☑ Relationship of force-deformation for rigid bar (in elasticity)

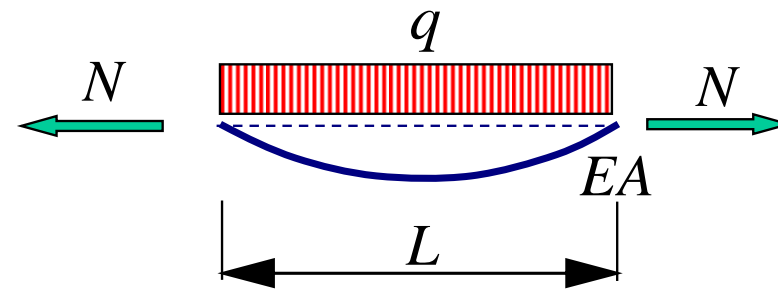
$$N = k \cdot u \rightarrow k = \text{Const}$$

- ☑ Relationship of force-deformation for cable

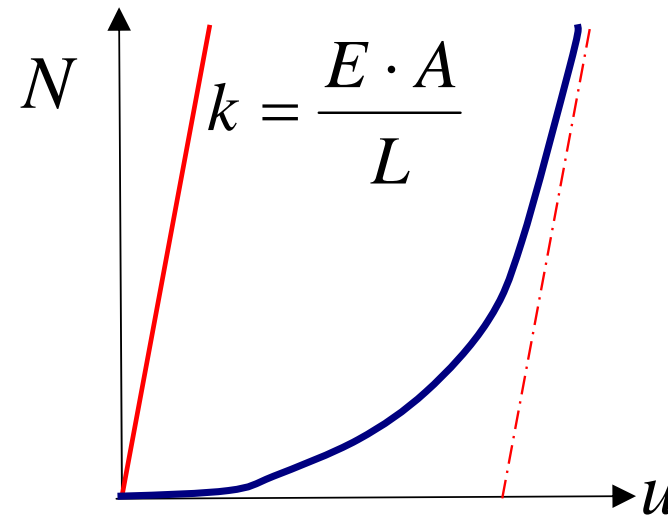
$$N = k(N) \cdot u \rightarrow k = \text{Variable}$$



Cable stiffness equation



$$k = \frac{E \cdot A}{L} \cdot \frac{1}{1 + \frac{E \cdot A \cdot L^2 \cdot q^2}{12N^3}}$$



Tension members

summary

- ☑ Resistance of cross-section
 - net section (in the same section)
 - section efficiency
 - three failure criteria
 - yield tension, yield moment and full plastic moment

- ☑ Rigidity of tension members
 - slenderness in two principal axis

- ☑ Characteristic of cable